

Effect of Tensile testing on behavioural shapes in AA6151 aluminium alloy

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Abstract:

This study investigates the effects of tensile testing on the mechanical behaviour and deformation characteristics of AA6151 aluminium alloy. AA6151, known for its favourable strength-to-weight ratio and excellent corrosion resistance, is widely used in aerospace, automotive and structural applications. Understanding its response to tensile stress is crucial for optimizing its performance in these applications.

In this research, standardized tensile tests were conducted on AA6151 specimens prepared according to ASTM guidelines. The tests were performed using a universal testing machine at a constant strain rate to obtain accurate stress-strain data. Key mechanical properties, such as yield strength, ultimate tensile strength and elongation at break, were determined from the stress-strain curves. Additionally, the study analyzed changes in the specimen shapes and surface characteristics post-testing to understand the deformation and failure mechanisms.

The results revealed significant insights into the alloy's elastic and plastic behaviour under tensile loading. The stress-strain curves indicated a clear yield point followed by strain hardening and eventual necking before fracture. The alloy exhibited a high degree of uniform elongation, indicative of its ductility. Micro-structural analysis post-fracture showed features typical of ductile failure, such as dimples and void coalescence. This study's findings enhance the understanding of AA6151's mechanical performance and provide valuable data for its application in design and engineering.

Keywords:

AA6151 aluminium alloy, Tensile Testing, Stress-Strain curve, Yield Strength, Ultimate tensile strength, Elongation, Deformation characteristics, Ductility and Fracture Mechanics.

1. Introduction:

Aluminium Alloys are widely recognized for their advantageous properties, including high strength-to-weight ratios, excellent corrosion resistance, and good formability. Among these, AA6151 aluminium alloy stands out due to its specific composition and performance characteristics, making it a preferred choice in aerospace, automotive and structural applications. Understanding the mechanical behaviour of AA6151 under various loading conditions is crucial for optimizing its use in engineering designs.

Tensile testing is a fundamental method employed to evaluate the mechanical properties of materials. By subjecting a materials to uniaxial tensile stress, it is possible to obtain critical information about its strength, ductility and deformation behaviour. This data is essential for predicting how the material will perform under real world conditions, where it might encounter various types of mechanical stress.

The purpose of this study is to investigate the effects of tensile testing on the behavioural shapes of AA6151 aluminium alloy. Specifically, this research aims to understand how the alloy deforms under tensile stress and to identify key mechanical properties such as yield strength, ultimate tensile strength and elongation at break.

Additionally, this study seeks to analyze the post testing deformation characteristics to gain insights into the material's failure mechanisms.

Previous research on aluminium alloys has highlighted the importance of mechanical testing in characterizing material behaviour. However, there is a need for more detailed studies focussing on AA6151, particularly concerning its response to tensile stress. This research aims to fill this gap by providing a comprehensive analysis of the tensile behaviour of AA6151, contributing to the broader understanding of its mechanical performance. In this study, AA6151 specimens were prepared and subjected to standardized tensile tests. The stress-strain data obtained from these tests were analyzed to determine the mechanical properties and deformation behaviour of the alloy.

1.1 Overview of AA6151 aluminium alloy and its applications:

AA6151 is an aluminium alloy belonging to the 6000 series, known for its combination of good mechanical properties, excellent corrosion resistance, and good workability. This alloy is primarily composed of aluminium, with magnesium and silicon as its major alloying elements. These elements contribute to its ability to be heat-treated to achieve medium to high strength levels, making it a versatile material for various applications.

1.1.1 Compositions:

- Aluminium (Al): Predominant element
- Magnesium (Mg): Typically around 0.6-0.9%
- Silicon (Si): Typically around 0.4-0.8%
- Other elements : Minor amounts of iron, copper, manganese, zinc and titanium may also be present in controlled quantities.

1.1.2 Properties:

- **Strength** : AA6151 offers medium to high tensile strength, which can be further enhanced through heat treatment.
- **Corrosion resistance**: Exhibits excellent resistance to atmospheric and marine environments, making it suitable for outdoor applications.
- **Weldability** : This alloy is known for its good weldability, especially using methods like MIG and TIG welding.
- **Workability**: It can be easily formed and machined, providing flexibility in manufacturing processes.
- **Tensile Strength**: approximately 250-350 Mpa (depending on temper)
- **Yield Strength**: approximately 150-300 Mpa (depending on temper)
- **Elongation**: 10-18% (depending on temper)
- **Hardness**: typically around 70-95 HB

The specific properties can vary based on the heat treatment and tempering process applied to the alloy.

Shape changes during tensile testing:- As the tensile load is applied to an AA6151 specimen, it undergoes significant shape changes:

1. **Elastic Deformation**:- Initially, the material deforms elastically, meaning it return to its original shape when the load is removed. This is represented by the linear portion of the stress-strain curve.
2. **Yield Point**:- Beyond the elastic limit, the material enters the plastic deformation region. At the yield point, the material begins to deform permanently.
3. **Necking**:- As the load increases further, the specimen begins to neck, or localize deformation to a specific region. This is due to the strain hardening effect, where the material becomes harder to deform as it is stretched.
4. **Fracture**:- Finally, the specimen fractures at the point of maximum necking.

Visual representation of shape changes



Fig. No.1 Visual representation of shape changes during tensile testing

Several factors can influence the shape changes observed during a tensile test of AA6151:

- **Specimen Geometry:** The shape and size of the specimen can affect the stress distribution and consequently the deformation behaviour.
- **Strain Rate:** The rate at which the load is applied can influence the material's response. Higher strain rates can lead to increased strength and reduced ductility.
- **Temperature:** Elevated temperatures can reduce the yield strength and increase ductility.
- **Material Microstructure:** The microstructure of the material, including grain size and precipitate distribution, can significantly affect its mechanical properties.

Several studies have focussed on AA6151 and similar aluminium alloys, such as those in the 6xxx series (Al-Mg-Si), investigating their mechanical properties, corrosion resistance, fatigue behaviour and fabrication processes. Below is an overview of some key studies and research areas:

1. Mechanical Properties and Microstructure Studies:

- **Study of Aging and heat treatment on AA6xxx series alloys:** Research has extensively covered the effects of various heat treatments (such as solution treatment and artificial aging) on the microstructure and mechanical properties of AA6151 and similar alloys. For instance, different temper such as T6 and T651 have been evaluated to optimize tensile strength, hardness and fatigue resistance.[Referred by Journal of Material Science]
- **Precipitation strengthening in Al-Mg-Si Alloy:** Investigations into the precipitation hardening process in Al-Mg-Si alloys, including AA6151, focus on the formation of Mg_2Si precipitates and their impact on strength and ductility. Studies on controlled aging temperatures and times show how these precipitates influence the alloy's mechanical performance.[Referred by Metallurgical and Materials Transactions]

2. Corrosion Resistance Studies:

- **Pitting corrosion in Al-Mg-Si alloys:** Research has highlighted the corrosion performance of AA6151 in marine and industrial environments. Pitting corrosion, influenced by chloride ions, is a significant concern for these alloys. Studies have shown how alloying elements and heat treatments affect the formation of passive films that protect against corrosion.[Referred by Corrosion Science]
- **Effect of Alloy composition on Corrosion Resistance:** Specific studies on the role of Mg and Si contents in the alloy have shown that higher magnesium levels improve corrosion resistance by enhancing the protective oxide layer. These studies compare AA6151 with other 6000 series alloys to assess corrosion behaviour in different environments.[Referred by Journal of Alloys and Compounds]

3. Fatigue and Fracture behaviour:

- **Fatigue Crack Growth in AA6000 Series Alloys:** Studies on fatigue crack initiation and growth in AA6151 have focused on the alloy's performance under cyclic loading, relevant to the aerospace and automotive industries. Crack propagation rates are influenced by the alloy's tensile properties, surface treatments and environmental conditions.[Referred by International Journal of Fatigue]
- **Effect on Corrosion fatigue on Al-Mg-Si Alloys:** The combined effects of corrosion and fatigue (corrosion fatigue) are a critical area of research. Studies have explored how exposure to corrosive environments effects the fatigue life of AA6151, providing insights into the alloy behaviour in marine and industrial applications. [Referred by Materials and Corrosion]

4. Welding and Joining Techniques:

- **Friction Stir Welding (FSW) of Al-Mg-Si Alloys:** FSW has been studied extensively for joining AA6000 series alloys, including AA6151. research has shown how FSW improves joint strength and corrosion resistance compared to traditional welding methods, with particular focus on the grain refinement and mechanical properties in the welded zones. [Refferd by Welding Journal]
- **Effects on welding on Tensile and fatigue properties:** Studies have focused on how different welding techniques, such as gas metal arc welding (GMAW) and friction stir welding, affect the tensile strength and fatigue life of AA6151 and similar alloys. These investigations are crucial for ensuring structural integrity in transportation and aerospace applications. [Referred by Journal of Materials Processing & Technology]

5. Applications in the Automotive and Aerospace Industries:

- **AA6151 for Automotive Components:** Research in automotive applications has looked into the suitability of AA6151 for structural parts, such as suspension system and chassis, where its combination of high strength and low weight is advantageous. Studies assess the alloy's performance in crash simulation, wear resistance, and thermal stability.[Referred by Journal of Automotive Engineering]
- **Aerospace Applications of AA6000 series alloys:** AA6151 has been evaluated for aerospace structural components due to its fatigue resistance and corrosion properties. Studies focus on how the alloy withstands operational withstand and environmental exposures typical in aircraft.[Referred by Aerospace Materials Journals]

6. Recycling and Sustainability of AA6151:

- **Recycling of AA6000 series alloys:** With an emphasis on sustainability, research has explored the recyclability of AA6151 and other 6000 series alloys. The studies analyze how recycled content affects mechanical properties and corrosion resistance, contributing to sustainable practices in the automotive and construction industries. [Referred by Journal of Sustainable Materials and Technologies]

2. Literature Review:

This study explores the restoration of tensile properties in PVD-TiN coated Al 7075-T6 alloy through post-heat treatment. Al 7075-T6, known for its high strength and lightweight characteristics, often experiences altered mechanical properties after the application of a physical vapour deposition (PVD) titanium nitride (TiN) coating. To address this, we subjected coated samples to various heat treatment regimes and conducted tensile tests to evaluate their mechanical properties. This results demonstrate that specific post heat treatment processes can effectively restore the tensile strength and ductility of PVD-TiN coated Al 7075-T6, making it suitable for high-performance applications where both surface hardness and core strength are critical.[1]

This study examines the potential and current limitations of in-situ fatigue testing within an environmental scanning electron microscope (ESEM). In-situ fatigue testing allows for real time observation of micro-structural changes under cyclic loading, providing valuable insights into fatigue mechanisms. However, ESEM's unique operating conditions, such as variable pressure and electron beam interactions, present challenges that can affect the accuracy and interpretation of results. Through a series of experiments, we identify the strength of

using ESEM for in-situ fatigue analysis and highlight key limitations, including resolution constraints and environmental control issues. Our findings underscore the need for continued advancements in ESEM technology to fully exploit its capabilities for fatigue research.[2]

This study evaluates the growth rate of small fatigue cracks in cast AM50 magnesium alloy, widely used for its lightweight and high strength properties, is susceptible to fatigue cracking, which can limit its structural applications. By conducting fatigue tests at different temperatures within a vacuum, we aim to isolate the thermal effects on crack propagation. The results indicate significant variations in crack growth rates with temperature changes, providing insights into the thermal fatigue behaviour of AM50. These findings contribute to a better understanding of the alloy's performance in temperature sensitive applications and help inform strategies for improving its fatigue resistance.[3]

This study presents an in-situ investigation of the pitting corrosion behaviour of friction stir welded (FSW) joints in AA2024-T3 aluminium alloy. Utilizing advanced microscopy techniques, we observed the initiation and progression of pitting corrosion in real time under controlled environmental conditions. The findings reveal distinct differences in corrosion susceptibility between the weld zone, heat-affected zone, and base material, highlighting the impact of the FSW process on corrosion resistance. These insights provide valuable information for improving the durability and performance of AA2024-T3 aluminium alloy joints in corrosive environments.[4]

This study models the crack propagation rate of corrosion fatigue under high frequency applied stress. By integrating environmental factors and mechanical loading conditions, the model aims to predict crack growth behaviour in materials subjected to corrosive environments. High frequency stress applications, often encountered in industrial components, exacerbate the rate of crack propagation due to the combined effects of mechanical fatigue and corrosion. The proposed model incorporates empirical data and theoretical frameworks to enhance the understanding of corrosion fatigue mechanisms. The results offer improved predictive capabilities for the life span of materials in high-stress, corrosive conditions, aiding the development of more durable and reliable engineering solutions.[5]

This study investigates the effect of prior corrosion on the behaviour of short cracks in 2024-T3 aluminium alloy. By subjecting pre-corroded samples to fatigue testing, we aim to understand how initial corrosion influences crack initiation and propagation. The findings reveal that prior corrosion significantly accelerates short crack growth, reducing the fatigue life of the alloy. Detailed analysis of the micro-structural changes and crack path morphology provides insights into the mechanisms driving this behaviour. These results underscore the critical impact of corrosion on the structural integrity of 2024-T3 aluminium alloy, highlighting the need for effective corrosion prevention measures in its applications.[6]

This study examines the role of tensile properties in the deformation behaviours of materials subjected to the equal channel angular extrusion process. ECAE is a severe plastic deformation technique, aims to enhance the mechanical properties of metals by refining their grain structures. By evaluating the tensile properties of Mg-3Al-Zn alloy before and after ECAE, we aim to understand how these properties influence the deformation mechanisms during the extrusion process. The findings demonstrate a significant correlation between initial tensile strength, ductility and the resulting micro-structural changes post-ECAE. This research provides valuable insights into optimizing ECAE parameters to achieve desired mechanical enhancements in various materials.[7]

This study explores the role of tensile properties in the influence of environmental factors on fatigue mechanisms in high temperature titanium alloy IMI834. By subjecting IMI834 to fatigue testing under various environmental conditions and temperatures, we aim to understand how tensile properties affect the alloy's fatigue behaviour. The findings indicate a significant interaction between tensile strength, ductility and environmental influences, such as oxidation and thermal effects, on crack initiation and propagation. These results provide critical insights into the durability and performance of IMI834 in high temperature applications, informing strategies for enhancing its fatigue resistance in challenging environments.[8]

This study investigates the micro-structure and corrosion performance of a cold-sprayed aluminium coating on AZ91D magnesium alloy. Cold spraying, a solid state coating process, was employed to deposit aluminium onto the magnesium substrate. Detailed micro-structural analysis revealed a dense and uniform aluminium coating with minimal porosity. Corrosion testing demonstrated a significant improvement in the corrosion resistance of the coated AZ91D alloy compared to the undercoated substrate. The findings highlight the potential of cold sprayed aluminium coatings to enhance the durability and lifespan of magnesium alloys in corrosive environments, making them suitable for a broader range of applications.[9]

This study investigates the surface fatigue micro-crack growth behaviour of cast Mg-Al alloy. By conducting fatigue tests on cast Mg-Al alloy specimens, we aimed to understand the initiation and propagation mechanisms of surface micro-cracks under cyclic loading. Detailed micro-structural analysis and crack growth monitoring were performed to observe the evolution of micro-cracks. The results indicate that surface micro-crack growth in cast Mg-Al alloy is significantly influenced by the alloy's micro-structural features and loading conditions. These insights contribute to a better understanding a fatigue behaviour in Mg-Al alloys, informing strategies to improve their fatigue resistance and structural integrity in engineering applications.[10]

This study investigates the initiation and propagation mechanisms of small cracks under low cycle fatigue (LCF) in cast magnesium alloys using in-situ observation with a scanning electron microscope (SEM). By subjecting cast magnesium alloy specimens to cyclic loading, we monitored the real time development of micro-cracks on the material's surface. The SEM observations provided detailed insight into the micro-structural factors influencing crack initiation and the subsequent growth behaviour. The findings reveal critical aspects of LCF behaviour, highlighting the role of micro-structural features such as grain boundaries and second phase particles in crack propagation. These results enhance the understanding of fatigue performance in cast magnesium alloys, aiding in the development of more durable materials for structural applications.[11]

This study presents in-situ observations of high cycle fatigue mechanisms in cast AM60B magnesium alloy under vacuum and water vapour environments. Using a scanning electron microscope (SEM), we monitored the real time behaviour of fatigue cracks to understand the effects of different environments on crack initiation and propagation. The findings reveal distinct differences in fatigue mechanisms between vacuum and water vapour conditions, with the latter significantly accelerating crack growth due to enhanced corrosion fatigue effects. These insights provide a deeper understanding of the environmental impact on the HCF performance of AM60B magnesium alloy, informing strategies to improve its durability in various applications.[12]

This study presents an SEM online investigation of fatigue crack initiation and propagation in cast magnesium alloy. By utilizing scanning electron microscopy (SEM), we observed the real time development of fatigue cracks under cyclic loading conditions. The investigation focussed on identifying the micro-structural features that influence crack initiation and subsequent propagation. Our findings reveal detailed insights into the behaviour of micro-cracks, including the role of grain-boundaries, inclusions, and second phase particles. This research enhances the understanding of fatigue mechanisms in cast magnesium alloys, contributing to improved material design and fatigue resistance in engineering applications.[13]

This study presents the direct observation of corrosion fatigue cracks in aluminium alloy using ultra-bright synchrotron radiation. By employing advanced synchrotron imaging techniques, we captured high resolution, real time images of crack initiation and propagation under simultaneous mechanical and corrosive conditions. The results reveal critical insights into the interaction between corrosion and fatigue mechanisms, highlighting the influence of environmental factors on crack growth rates and paths. This research advances the understanding of corrosion fatigue behaviour in aluminium alloys, providing valuable information developing more durable materials for use in corrosive environments.[14]

This study investigates the role of tensile properties in the initiation and growth behaviour of short fatigue cracks emanating from a single edge notch specimen, using in-situ scanning electron microscopy (SEM). By conducting tensile tests and fatigue cycling on the specimens, we observed the real time development of short cracks. The SEM analysis provided detailed insights into the micro-structural factors and tensile properties

influencing crack initiation and propagation. The results demonstrate a significant correlation between initial tensile properties, such as strength and ductility, and the behaviour of short fatigue cracks. These findings enhance the understanding of fatigue mechanisms in notched specimens, contributing to the development of materials with improved fatigue resistance.[15]

This study explores the role of tensile properties in the fatigue crack growth behaviour of IN718 nickel-based super alloy using in-situ scanning electron microscopy (SEM). By performing tensile and cycling loading tests on IN718 specimens, we monitored the real time real initiation and propagation of fatigue cracks. Detailed SEM observations revealed the micro-structural factors and tensile properties that influence crack growth rates and paths. The results show a significant relationship between the alloy's tensile strength, ductility and its fatigue crack growth behaviour. These insights contribute to a deeper understanding of the fatigue performance of IN718, aiding in the optimization of its mechanical properties for high-stress applications.[16]

This study examines the role of tensile properties in the propagation of corrosion in AA2024-T3 aluminium alloy. As part of a broader investigation, this third segment focuses on how variations in tensile strength and ductility influence the progression of corrosion induced damage. By subjecting AA2024-T3 specimens to tensile testing followed by exposure to corrosive environments, we observed the development and growth of corrosion features. The findings indicate that tensile properties significantly affect the rate and morphology of corrosion propagation, with higher tensile strengths generally slowing down the corrosion spread. These insights are crucial for enhancing the durability and performance of AA2024-T3 in corrosive applications.[17]

This study investigates the role of tensile properties on the interaction between prior corrosion and fatigue behaviour in 2024-T3 aluminium alloy. By subjecting pre-corroded specimens to tensile and fatigue testing, we aimed to understand how initial tensile properties influence crack initiation and propagation under cyclic loading. The results reveal that tensile strength and ductility significantly affect the fatigue life of pre-corroded 2024-T3 alloy, with higher tensile properties generally improving resistance to crack growth. Detailed micro-structural analysis provided insights into the mechanisms driving this behaviour. These findings contribute to a better understanding of the combined effects of corrosion and fatigue on 2024-T3 aluminium alloy, informing strategies for improving its durability in structural applications.[18]

This study explores the role of tensile properties in the pitting corrosion and fatigue crack nucleation in aluminium alloys, and examines the effects of the environment on crack initiation and growth. By conducting tensile and fatigue tests on pre-corroded specimens under varying environmental conditions, we aimed to understand how tensile strength and ductility influence the onset and propagation of fatigue cracks from corrosion pits. The findings reveal that higher tensile properties generally enhance resistance to crack initiation and growth. Environmental factors, such as humidity and corrosive agents, significantly accelerate crack nucleation and propagation. These insights contribute to a comprehensive understanding of the interplay between mechanical properties, corrosion and environmental conditions, informing strategies to improve the durability and performance of aluminium alloys in demanding applications.[19]

This study investigates the role of tensile properties in predicting the fatigue crack initiation life based on pit growth in aluminium alloys. By analyzing the relation between the tensile strength, ductility and the developments of corrosion pits, we aim to establish a predictive model for fatigue crack initiation life. The findings demonstrate that tensile properties significantly influence the rate of pit growth and subsequent crack initiation under cyclic loading. The proposed model incorporates tensile properties to accurately forecast the fatigue life of pre-corroded specimens. These insights are crucial for enhancing the reliability and lifespan of aluminium alloys in corrosive environments.[20]

This study examines the role of tensile properties in the pit-to-crack transition of pre-corroded 7075-T6 aluminium alloy under cyclic loading. By subjecting pre-corroded specimens to fatigue testing, we aim to understand how tensile strength and ductility influence the transition from corrosion pits to fatigue cracks. The

results reveal that higher tensile properties delay the pit-to-crack transition, enhancing the alloy's resistance to fatigue crack initiation. Detailed micro-structural analysis provided insights into the mechanisms driving this behaviour. These findings contribute to a better understanding of the interplay between mechanical properties and corrosion damage, informing strategies to improve the fatigue performance of 7075-T6 aluminium alloy in corrosive environments.[21]

This study examines the role of tensile properties in the fatigue crack growth from corrosion damage in 7075-T6511 aluminium alloy under aircraft loading conditions. By exposing pre-corroded specimens to cyclic loading that mimics the stresses experienced during aircraft operations, we analyzed how tensile strength and ductility affect the progression of fatigue cracks initiated by corrosion damage. The results indicate that higher tensile properties enhance resistance to crack growth, thereby improving the alloy's durability. Detailed micro-structural evaluations provided insights into the underlying mechanisms. These findings are essential for predicting the fatigue performance and ensuring the reliability of 7075-T6511 aluminium alloy in aerospace applications.[22]

This study develops a fracture model for corrosion fatigue crack propagation in aluminium alloys, emphasizing the role of tensile properties and the fracture of material elements ahead of a crack tip. By integrating the tensile strength and ductility parameters into the model, we aim to predict the progression of corrosion induced fatigue cracks. The model considers the micro-structural damage and fracture mechanisms occurring in the material elements directly ahead of the crack tip. Experimental validation involved subjecting pre-corroded aluminium alloy specimens to cyclic loading and observing crack growth behaviour. The results demonstrate that tensile properties significantly influence crack propagation rates and patterns. This model enhances the understanding of corrosion fatigue mechanisms, providing a valuable tool for predicting the durability of aluminium alloys in corrosive environments.[23]

This study investigates the role of tensile properties in the micro-fracture characteristics of concrete at various temperature values using online scanning electron microscopy (SEM). By subjecting concrete specimens to tensile testing across a range temperature, we monitored real time fracture development at the micro-scale. The SEM observations provided detailed insights into how tensile strength and ductility influence the initiation and propagation of micro-fractures under thermal stress. The findings reveal significant variations in fracture behaviour with temperature changes, highlighting the critical impact of tensile properties on concrete's performance in different thermal environments. These insights are essential for optimizing the durability and structural integrity of concrete in temperature sensitive applications.[24]

This study explores the role of tensile properties in the high cycle fatigue behaviour of SnPb solder joints in electronic packaging through an in-situ scanning electron microscopy (SEM) investigation. By subjecting SnPb solder joints to cyclic loading, we observed real time crack initiation and propagation under high cycle fatigue conditions. The SEM analysis provided detailed insights into the influence of tensile strength and ductility on the fatigue performance of the solder joints. The findings reveal that tensile properties significantly impact crack growth rates and failure mechanisms. These insights are crucial for enhancing the reliability and longevity of electronic packaging, informing the development of more robust solder joints materials.[25]

This study characterizes the role of tensile properties in the growth of fatigue surface micro-cracks in vicinal inclusions within powder metallurgy alloys. By conducting tensile and fatigue tests on specimens, we analyzed how variations in tensile strength and ductility influence the initiation and propagations of micro-cracks near inclusions. Detailed observations and measurements were made using advanced microscopy techniques to understand the micro-structural interactions at play. The results demonstrate a significant correlation between tensile properties and the rate of micro-crack growth, providing critical insights into the fatigue behaviour of powder metallurgy alloys. These findings are essential for optimizing alloy design and processing to enhance fatigue resistance in structural applications.[26]

This study investigates the effect of tensile properties on fatigue crack initiation at a notch. By subjecting notched specimens with varying tensile strengths and ductilities to cyclic loading, we aimed to understand how these properties influence crack initiation behaviour. The findings reveal a significant correlation between tensile properties and the ease of crack initiation, with higher tensile strength and ductility generally leading to improved resistance to crack formation. Detailed micro-structural analysis provided insights into the mechanism driving this behaviour. These results are crucial for optimizing material properties to enhance fatigue performance in notched components.[27]

This study investigates the role of tensile properties on the effect of pitting corrosion on very high cycle fatigue behaviour in metals. By exposing specimens with varying tensile strengths and ductilities to corrosive environments, followed by cyclic loading tests, we aimed to understand how tensile properties influence the initiation and propagation of fatigue cracks from corrosion pits. The results indicate that higher tensile strength and ductility improve resistance to fatigue crack initiation and growth, even in the presence of pitting corrosion. Detailed micro-structural analysis revealed the mechanisms behind the observed behaviour. These findings are critical for predicting the very high cycle fatigue performance of materials in corrosive environments and for developing strategies to enhance their durability.[28]

3. Materials and Methods:

3.1 Materials Preparation: Details on the AA6151 samples used, including their composition and treatment.

3.1.1 Composition of AA6151 samples:

Typical elemental composition of AA6151 alloy includes:

Aluminium (Al): Balance

Magnesium (Mg): 0.6-0.9% (improves strength and corrosion resistance)

Silicon (Si): 0.6-0.9% (promotes precipitation strengthening)

Manganese (Mn): 0.2-0.6% (enhances strength and toughness)

Chromium (Cr): 0.15% (improves corrosion resistance and strength)

Zinc (Zn): 0.25% max(trace)

Copper (Cu): 0.10% max (trace)

Titanium (Ti): 0.10% max (trace)

These precise concentrations are crucial, as they impact the mechanical properties, corrosion resistance and response to heat treatment.

3.2 Heat treatment and Temper conditions:

The heat treatment process used for AA6151 samples varies based on the desired mechanical properties and experimental requirements:

- **Solution Heat Treatment:** The samples are first subjected to solution treatment at around 530-550°C for 1-2 hours.

- **Quenching:** Post solution treatment, the samples are quenched rapidly, typically in water at room temperature, to “freeze” the elements in the solid solution state. This creates a supersaturated solid solution essential for precipitation hardening.

- **Aging Treatment:**

- 3.2.1 Artificial Aging (T6 or T651 condition):** For peak hardness and strength, the samples are aged at temperature around 160-180°C for 8-10 hrs.

- 3.2.2 Natural Aging (T4 condition):** If a lower hardness level is preferred, the alloy may be aged naturally at room temperature for several days to achieve desired properties with more ductility.

3.3 Mechanical Processing of Samples:

After heat treatment, samples are often machined and prepared based on the experimental requirements. Typical preparation steps include:

- **Cutting and Shaping:** Samples are machined to standard shapes, such as cylindrical or rectangular bars for tensile testing, and compact tension specimens for fracture and fatigue testing.

- **Surface Penetration:** Samples are polished with progressively finer abrasives, commonly from 320 to 1200 grit, to obtain a smooth surface. Final polishing with diamond pastes or alumina suspensions may be performed for micro-structural analysis.
- **Cleaning:** Samples are cleaned with ethanol or acetone to remove any contaminants before testing.

3.4 Standard Sample Dimensions:

- **Tensile Test Samples:** Dog-bone-shaped specimens are commonly used, with a gauge length of 25mm and a width of 6 mm, following ASTM E8 standards.
- **Fracture and Fracture Test Samples:** Compact tensions (CT) specimens or single-edge notched specimens are typically used, with notch dimensions following ASTM E647 standards.

4. Equipment, Set-up and conditions for a tensile test on AA6151 Aluminium Alloy:-

Equipment:

4.1 Universal Testing Machine (UTM):

- A versatile machine capable of applying tensile, compressive and flexural loads.
- **Essential Components:**
- Load Frame: A rigid structure to support the test specimen and apply the load.
- Load Cell: Measures the applied load with high accuracy.
- Cross Head: A movable part that applies the load to the specimen.
- Extensometer: Measures the elongation of the specimen during the test.

4.2 Tensile test Specimen:

- A precisely machined specimen conforming to a specific standard (e.g. ASTM E8/E8M) to ensure consistent results.
- Typically, a dumbbell shaped specimen with a reduced gauge section for accurate stress calculations.

Set-up:

4.3 Specimen Preparation:

- Machine the specimen to the required dimensions, ensuring smooth surfaces and sharp edges.
- Clean the specimen to remove any contaminants that may affect the test results.

4.4 Mounting the specimen:

- Secure the specimen in the grips of the UTM, ensuring proper alignment and minimal stress concentrations.
- Use appropriate grips to prevent slippage and premature failures.

4.5 Extensometer Attachment:

- Attach the extensometer to the gauge length of the specimen to measure strain accurately.

4.6 Test Parameter Selection:

- Set the desired crosshead speed (strain rate) according to the testing standards or specific requirements.
- Configure the UTM to record load and elongation data at appropriate intervals.

Test Conditions:

- **Ambient Temperatures:** The test is typically conducted at room temperature around 23°C.
- **Humidity:** Controls humidity levels to prevent significant moisture effects on the material's properties.
- **Strain rate:** The rate at which the load is applied, expressed at the strain rate (e.g. mm/min. or in/min). This can influence the material's behaviour, particularly its ductility and strength.

Data Acquisition and Analysis:

- The UTM's data acquisition system records the load and elongation data during the test.
- The data is then used to plot a stress-strain curve, from which various mechanical properties can be determined, including:
 - Yield Strength
 - Ultimate tensile strength
 - Elongation
 - Modulus of elasticity

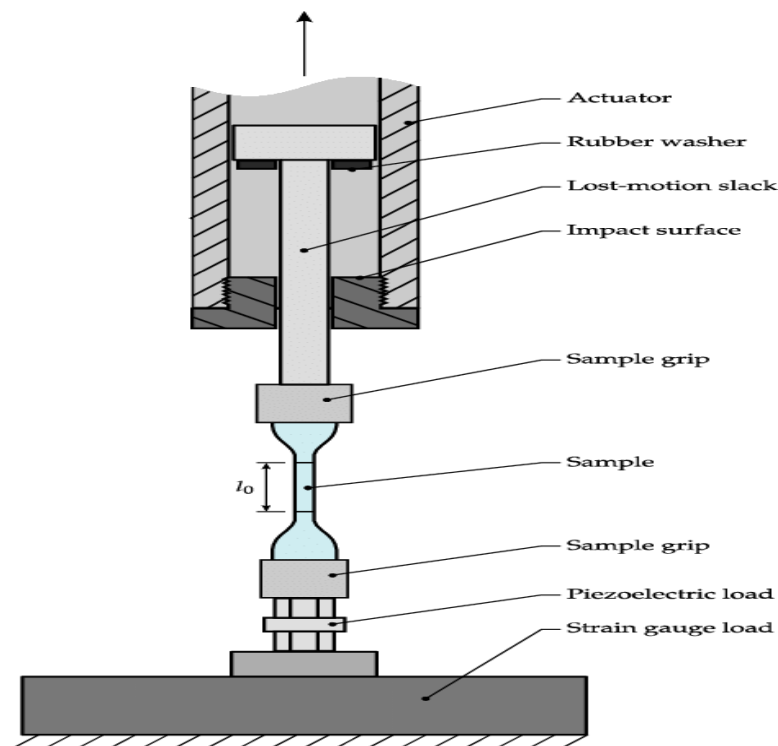


Fig. No. 2 Set-up diagram of tensile test specimen

Tensile testing dramatically alters the shape of an AA6151 aluminium alloy specimen, and these changes are directly reflected in the stress-strain curve. Here's a breakdown of how the shape changes relate to the curve:

4.7 Elastic region (linear portion of the curve):-

- **Shape change:** The specimen elongates uniformly along its gauge length. There's no permanent deformation; if the load were removed, the specimen would return to its original dimensions.
- **Stress-Strain curve:** This is the straight -line portion of the curve, where stress and strain are proportional (Hooke's law). The slope of this line is the modulus of elasticity (Young's modulus), indicating the material's stiffness.

4.8 Yield Point:-

- **Shape Change:** The specimen begins to deform permanently (plastically). This marks the transition from elastic to plastic deformation.

- **Stress-Strain curve:** This is the point where the curve deviates from linearity. The stress at this point is the yield strength.

4.9 Strain Hardening Region:-

- **Shape change:** The specimen continues to elongates, and the cross-sectional area start to decrease slightly. The material becomes stronger due to dislocation movement and interaction within its crystal structure.
- **Stress-Strain Curve:** The curve continues to rise, but with a decreasing slope. This region shows the material's ability to withstand increasing stress as it deforms plastically.

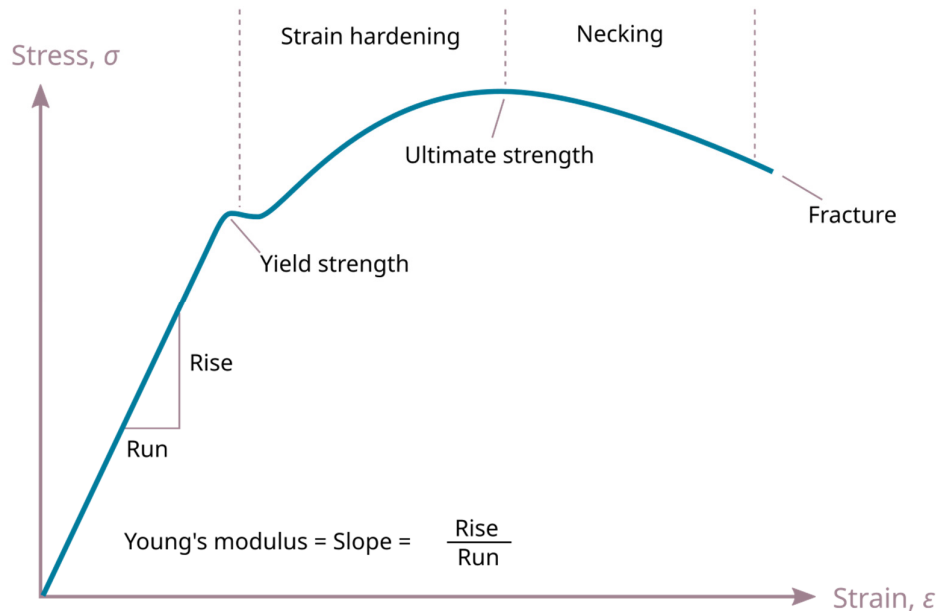


Fig No.3 Stress-Strain Curve with labelled regions and corresponding specimen shapes

4.10 Ultimate Tensile Strength (UTS):-

- **Shape change:** The specimen reaches its maximum load bearing capacity. At this point, necking begins to occur, where the deformation becomes localized to a smaller region of the specimen.
- **Stress –Strain curve:** This is the peak point on the curve, representing the maximum stress the material can withstand.

4.11 Necking Region:-

- **Shape Change:** A distinct localized reduction in the cross-sectional area (neck) forms in the specimen. This is a sign of impending failure.
- **Stress-Strain curve:** After reaching the UTS, the stress on the curve starts to decrease as the localized deformation at the neck accelerates.

4.12 Fracture Point:-

- **Shape change:** The specimen breaks at the neck.
- **Stress-Strain curve:** This is the final point on the curve, representing the stress at which the material fractures.

In summary, The tensile test and the resulting stress-strain curve provide a comprehensive understanding of how AA6151 deforms and eventually fails under tensile loading. By correlating the shape changes with the different regions of the stress-strain curve, engineers can gain valuable insights into the material's behaviour and its suitability for various applications.

5. Results and Discussion of a Tensile Test on AA6151 Aluminium Alloy:-

When a tensile test is performed on AA6151, a stress strain curve is generated, and key mechanical properties are determined. Typical results for AA6151 in the T6 temper (a common heat treatment) include:

- Yield Strength : Around 275 MPa (40 ksi)
- Ultimate Tensile Strength : Around 310 MPa (45 ksi)
- Elongation at fracture: Around 12-15%

Property	Value (Metric)	Value (Imperial)
Yield Strength (YS)	~275 MPa	~40 ksi
Ultimate Tensile strength (UTS)	~310 MPa	~45 ksi
Elongation at fracture	~12-15%	~12-15%
Modulus of Elasticity (E)	~70 GPa	~10×10 ⁶ psi

Table No.1 Typical tensile test results for AA6151-T6 Aluminium Alloy

Actual experimental results may vary due to factors like:

- Specimen Geometry: The shape and dimensions of the test specimen.
- Strain rate : The rate at which the load is applied.
- Testing Temperature : Although typically done at room temperature, variations can occur.
- Materials Processing: Variations in the manufacturing process can affect the microstructure and thus the mechanical properties.

Here's a representative stress-strain curve graph for AA6151-T6,

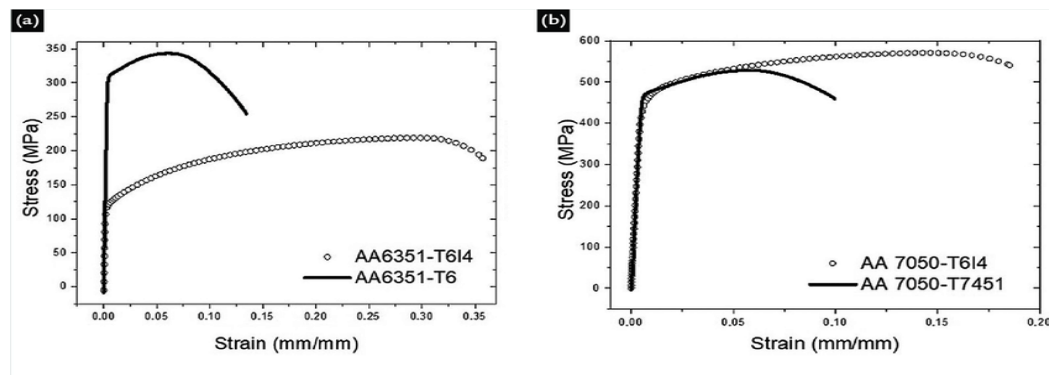


Figure No. 4 stress-strain curve graph for AA6151-T6

Key features and its explanations:

- **X-axis: Strain (ϵ)** – Represents the deformation of the material, expressed as a percentage or as a dimensionless value (change in length divided by original length)

- **Y-axis: Stress (σ)** – Represents the force applied per unit area of the material, typically measured in MPa or ksi (kilo pounds per square inch).

5.1 Regions of the curve:

5.1.1 Elastic region (O to A):

- This is the initial linear portion of the curve.
- Stress is directly proportional to strain.
- The slope of this line is the modulus of elasticity (E), representing the material's stiffness.
- If the load is removed within this region, the material will return to its original shape.

5.1.2 Yield Point (A):

- This is the point where the curve starts to deviate from linearity.
- It marks the transition from elastic to plastic deformation.
- The stress at this point is the Yield Strength (YS), indicating the stress at which the material begins to deform permanently.

5.1.3 Strain Hardening Region (A to B):

- Beyond the yield point, the material continues to deform plastically and the stress increases with increasing strain.
- This is due to dislocation movement and interactions within the material's microstructure.

5.1.4 Ultimate Tensile Strength (UTS) (B):

- This is the peak point on the curve, representing the maximum stress the material can withstand before necking begins.

5.1.5 Necking Region (B to C):

- After reaching the UTS, the cross-sectional area of the specimen starts to decrease locally (necking).
- The stress on the curve decreases as the localized deformation accelerates.

5.1.6 Fracture Point (C):

- This is the point where the specimen breaks.
- The stress at this point is the fracture strength.

Important Considerations:

- The shape and specific values of the stress-strain curve can vary depending on factors like the material's temper (heat treatment), processing history, testing temperature and strain rate.
- The curve shown is a typical representation for AA6151-T6, which is a common temper. Other tempers will have different curves and mechanical properties.

It's challenging to provide a precise microstructure diagram without having access to specific metallographic images of AA6151 samples. However, I can offer a representative diagram and explain the key microstructural features typically observed in this alloy, especially in the T6 temper.

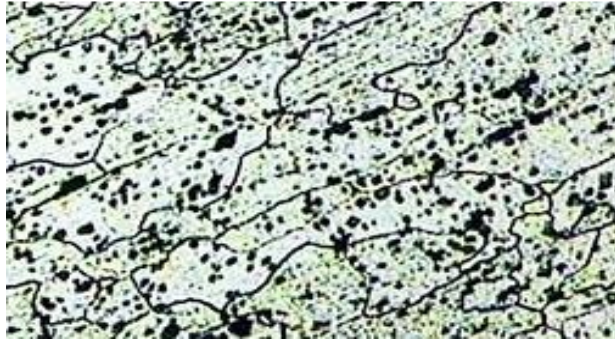


Figure No.5 Representative microstructure diagram for AA6151-T6

Key Micro-structural Features:

1. Aluminium matrix (α -Al):

- This is the primary phase, forming the background of the microstructure.
- It consists of aluminium atoms arranged in a face-centered cubic (FCC) crystal lattice.

2. Mg_2Si precipitates:

- These are the primary strengthening precipitates in AA6151.
- They form during the artificial aging process (T6 temper) as fine, coherent particles dispersed throughout the aluminium matrix.
- These precipitates hinder dislocation movement, increasing the alloy's strength and hardness.

3. Grain Boundaries:

- These are the interfaces between individual aluminium grains.
- They can influence the material's strength and ductility.
- In AA6151, the grain size is typically controlled during processing to optimize mechanical properties.

Relationship to Mechanical properties:

- **Fine Mg_2Si precipitates:** These are crucial for achieving high strength in AA6151-T6. Their size, distribution, and coherency with the matrix directly affect the alloy's yield strength and ultimate tensile strength.
- **Grain size:** Smaller grain sizes generally lead to higher strength due to increased grain boundary area, which hinders dislocation movement.
- **Other Inter-metallic particles:** Depending on the specific composition and processing, other intermetallic particles may be present in smaller amounts. These can have varying effects on the alloy's properties.

Micro-structural Analysis Techniques:

- **Optical Microscopy:** Used to observe the grain structure and larger precipitates.
- **Scanning Electron Microscopy (SEM):** Provides higher magnification images to reveal finer details of the micro-structure, including the size and distribution and Mg_2Si precipitates.
- **Transmission Electron Microscopy (TEM):** Offers the higher magnification, allowing for detailed analysis of the crystal structure and coherency of the precipitates.

Effect of Heat-Treatment:

- **Solution Heat Treatment:** This involves heating the alloy to a high temperature to dissolve the alloying elements (Mg and Si) into a solid solution.

- **Quenching:** Rapid cooling traps the alloying elements in a supersaturated solid solution.
- **Artificial Aging (T6 temper):** Heating the quenched alloy to an intermediate temperature allows the Mg and Si atoms to precipitate out as fine Mg_2Si particles, leading to strengthening.

Conclusion:

Tensile testing provides a comprehensive understanding of how AA6151-T6 aluminium alloy behaves under tensile loading, revealing crucial information about its mechanical properties and deformation characteristics. The key findings and their interrelationships are summarized below:

- **Deformation Behaviour and the Stress Strain curve:** The tensile test directly demonstrates the relationship between applied stress and resulting strain. The stress-strain curve vividly illustrates the different stages of information:
 - **Elastic Region:** Uniform elongation with no permanent deformation. The slope of this region(Young's modulus) indicates the material's stiffness.
 - **Yield Point:** The onset of plastic deformation, marking the transition from elastic to permanent deformation. The stress at this point is the yield strength.
 - **Strain Hardening:** Continued plastic deformation with increasing stress due to dislocation interactions.
 - **Ultimate Tensile Strength (UTS):** The maximum stress the material can withstand before necking.
 - **Necking:** Localized reduction in cross-sectional area, leading to eventual fracture.
 - **Fracture:** The point at which the material breaks.
- **Mechanical Properties:** The tensile test quantifies key mechanical properties:
 - **Yield Strength (YS):** Approximately 275 MPa (40 ksi) for AA6151-T6.
 - **Ultimate Tensile Strength (UTS):** approximately 310 MPa (45 ksi) for AA6151-T6.
 - **Elongation at Fracture:** Typically around 12-15%, indicating good ductility.
 - **Modulus of Elasticity (E):** approximately 70 GPa (10×10^6 psi), representing the material's stiffness.
- **Micro-Structural Influence:** The micro-structure of AA6151-T6, particularly the presence of fine Mg_2Si precipitates within the aluminium matrix, plays a critical role in its mechanical properties. These precipitates impede dislocation movement, resulting in increased strength and hardness. The T6 temper, achieved through solution heat treatment and artificial aging, optimizes the size and distribution of the precipitates.
- **Shape changes during testing:** The visible shape changes during the tensile test directly correlate with the stress-strain curve:
 - Uniform elongation in the plastic region.
 - Onset of localized deformation (necking) near the UTS.
 - Final fracture at the neck.
- **Practical Implications:** The combination of moderate strength, good ductility and excellent corrosion resistance makes AA6151-T6 suitable for various applications in automotive, aerospace, construction and general engineering. The data obtained from tensile testing is essential for design engineers to ensure structural integrity and performance of components made from this alloy.

Future Prospects: The future prospects for AA6151-T6 aluminium alloy appear promising about our methods of observing and understanding the shape changes in AA6151 during tensile test will evolve. Some following points mentioned below with various applications:

1. Enhanced Visualization and Measurement:

- **4D Imaging:** Combining 3D imaging techniques (like X-Ray tomography) with time-resolved measurements will enable 4D visualization of the deformation process. This will provide unprecedented detail about how the material deforms internally, including the initiation and propagation of cracks.

- **High Speed Cameras and Advanced Optics:** Using High Speed Cameras and Advanced Optical techniques (like interferometry) will allow for more precise measurement of surface deformation and strain localization during the tensile test, especially during the rapid necking and fracture stages.
- **Digital Image Correlations (DIC) Enhancements:** DIC techniques will continue to improve, with higher resolution, faster acquisition rates and ability to measure deformation in more challenging environments(e.g. high temperatures).

2. Linking shape change to micro-structure:

- **In-Situ Micro-structural Observation:** Combining tensile testing with in-situ techniques like electron microscopy or X-Ray diffraction will allow for direct observation of micro-structural changes (e.g., dislocation movement, precipitate deformation) as the material deforms. This will establish a stronger link between the observed shape changes and the underlying micro-structural mechanisms.
- **Crystal Plasticity Modeling:** Advanced computational models that incorporate crystal plasticity theory will be used to simulate the deformation behaviour of AA6151 at the micro-structural level. This will help to predict and understand the observed shape changes based on the material's micro-structure.

3. Artificial Intelligence and Machine Learning:

- **Automated shape analysis:** Machine learning algorithms can be trained to automatically analyze images and videos of tensile tests, extracting quantitative information about shape changes, such as necking geometry and crack propagation.
- **Predictive modelling shape evolution:** Machine learning models can be used to predict the shape changes of AA6151 under different loading conditions based on experimental data and micro-structural information.

4. Application specific insights:

- **Additive Manufacturing:** Understanding the shape changes during tensile testing of additively manufactured AA6151 components will be crucial for optimizing printing parameters and ensuring structural integrity.
- **Welding and Joining:** Analyzing the deformation behaviour of welded or joined AA6151 structures will help to improve welding techniques and predict the performance of these joints under load.

Data Transparency

Authors will ensure data transparency.

Acknowledgements all authors would like to acknowledge to encourage our publication work and more give guidance to me about research facilities for the present work.

Authors contribution All authors contribute equally to the manuscript.

Funding No funding was received for conducting this study.

Data availability All data generated or analyzed during this study are included in this published articles.

Declarations

Conflict of interest The authors have no relevant financial or non-financial interests to disclose.

Ethical Approval Not applicable.

Consent to participate Not applicable

Consent for publication Not applicable

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